

# An Experimental and Finite Element Study of the Porcine Carotid Artery Under Dynamic Loading

F. Scott Gayzik<sup>1,2</sup>, Ola Bostrom<sup>3</sup>, Per Örtengren<sup>4</sup>,  
Stefan M. Duma<sup>1</sup>, Joel D. Stitzel<sup>1,2</sup>  
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<sup>1</sup> Virginia Tech – Wake Forest University Center for Injury Biomechanics  
<sup>2</sup> Wake Forest University School of Medicine  
<sup>3</sup> Autoliv Research, Vargada, Sweden  
<sup>4</sup> Sahlgrenska University Hospital, Gothenburg, Sweden

## Center for Injury Biomechanics

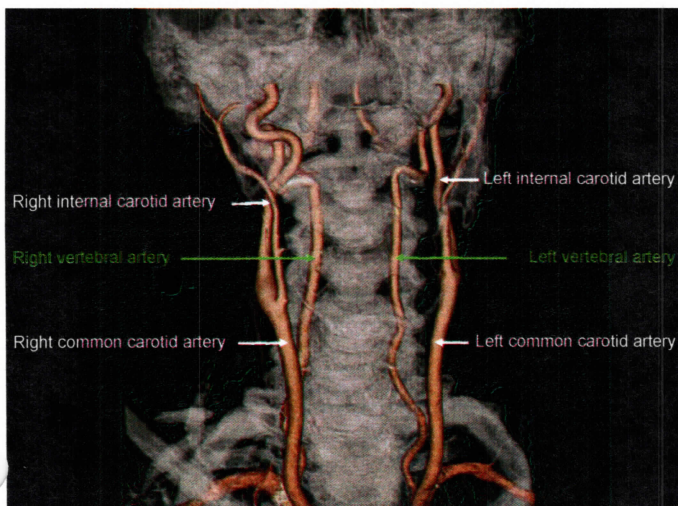
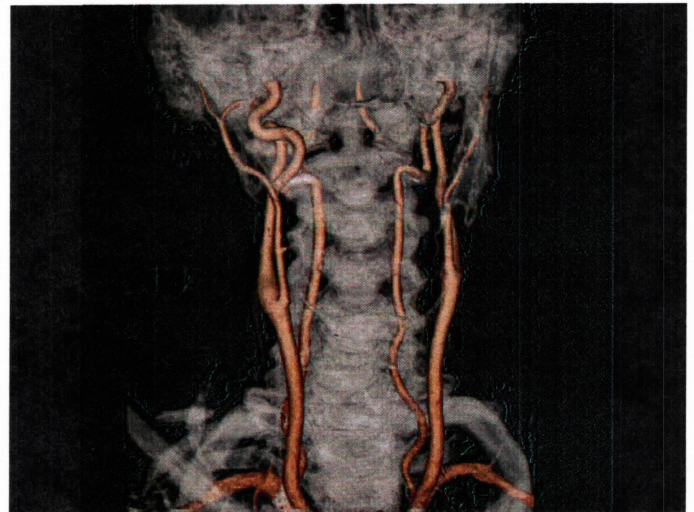


## Study motivation and hypothesis

- Experiment: Blunt impact to porcine carotid arteries → intimal-side damage
- Simulation: Use finite element method to determine dynamic strains within the vessels during this experiment
  - How do computed strain values compare to what is known about carotid artery injury?

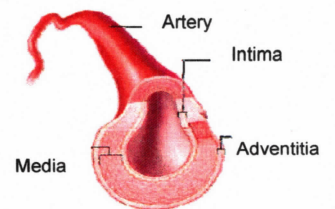
## Blunt cerebrovascular injury (BCVI)

- Blunt injury to either carotid or vertebral arteries
- Uncommon injury, but potentially devastating consequences
  - 1% of trauma admissions
  - Mortality(40%), morbidity(40-80%)
- Injury causation
  - Car crash, stretching
- Injury mechanisms (regional level)
  - Blunt impact, hyperextension / rotation, skull / vertebral body fracture
- Injury mechanisms (tissue level)
  - tension, pinching (intima-intima contact)

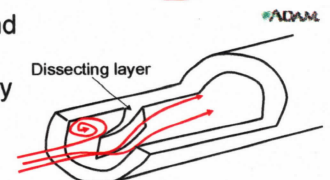


## Pathophysiology and study goals

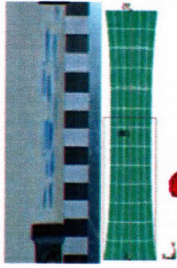
**Intimal Damage**  
 ↓ Thrombosis  
 Dissection  
 ↓ Embolism  
 Occlusion



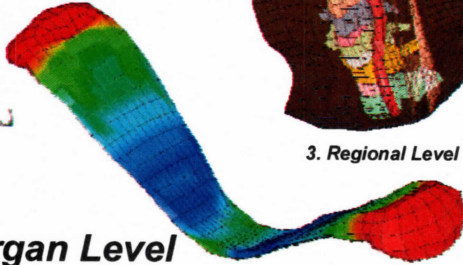
- **Study Goal:** Develop and validate an *organ level* model of the carotid artery for prediction of strain to intimal damage



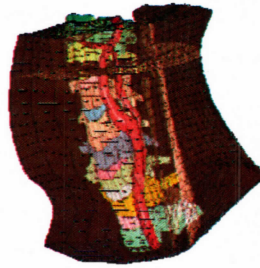
## FE model development strategy



1. Tissue Level



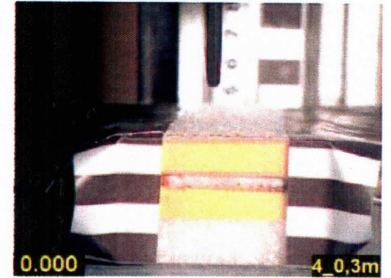
2. Organ Level



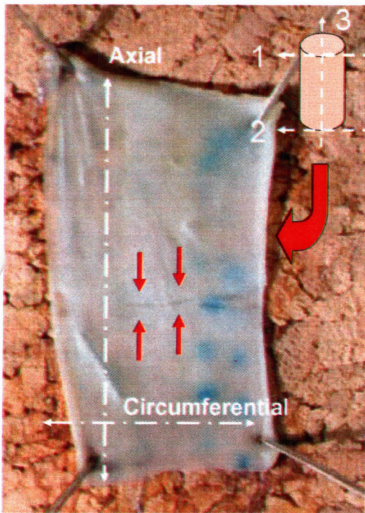
3. Regional Level

## Experimental protocol for blunt impact test

- Porcine carotid arteries
  - Impacted from 3 heights
  - Indenter motion stopped by foam (no sudden stop)
  - Saline filled, (zero gauge pressure)
  - Free end conditions
- Data from experiment
  - Video of drop
  - Percent injury based on drop height



2.4 kg steel indenter,  
5 mm beveled tip

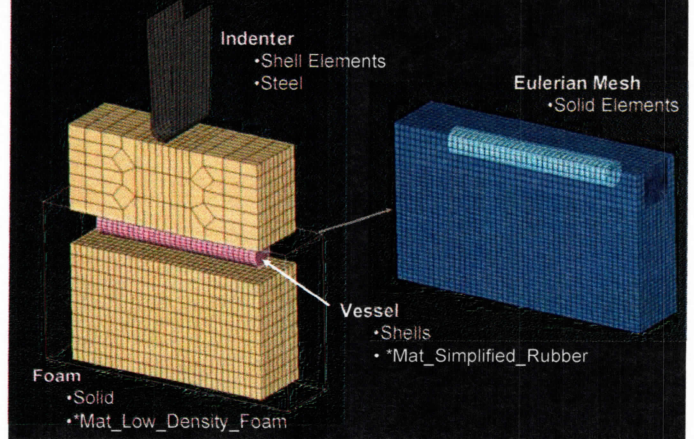


## Experiment results

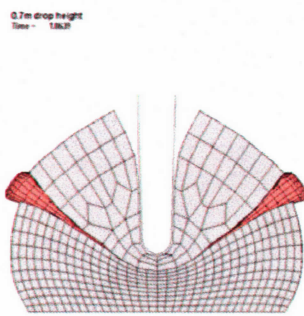
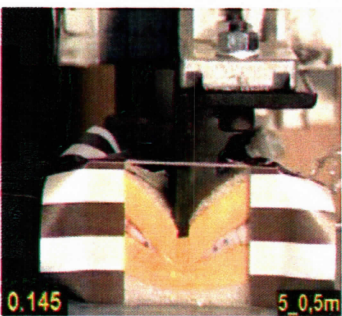
Drop Height (m)	Impact Velocity (m/s)	n tests	Injury frequency
0.3	2.4	2	0%
0.5	3.1	4	25%
0.7	3.7	4	100%

Used to develop FE model

## Finite element model of experiment

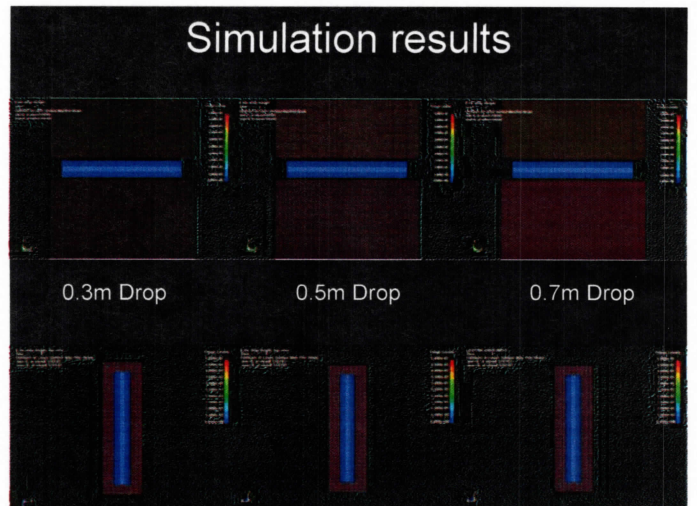


## Boundary conditions and validation procedures

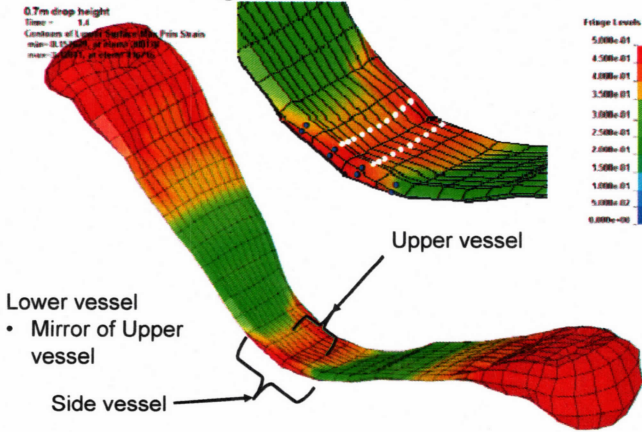


- Mesh constructed from video of impact test (*imageJ, NIH*)
- Validation procedures conducted by tracking indenter and foam motion on high speed video

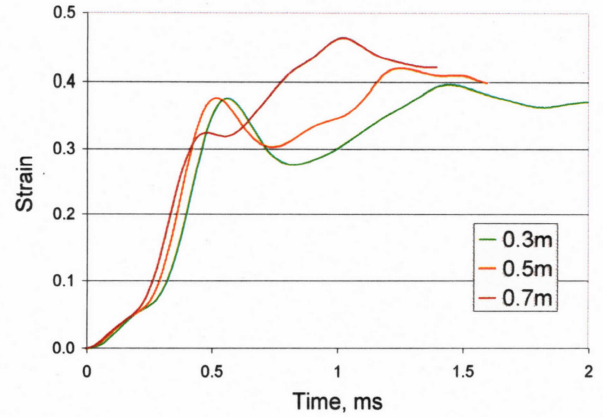
## Simulation results



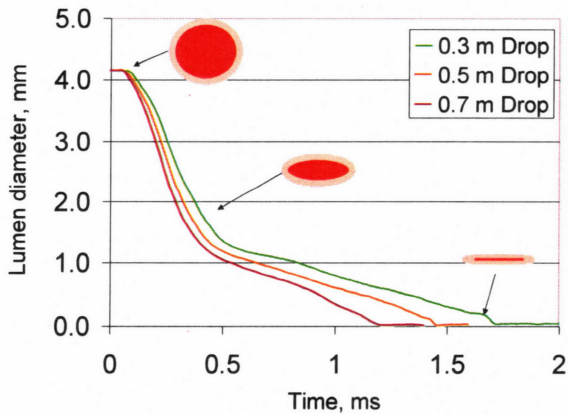
## Regions of Interest



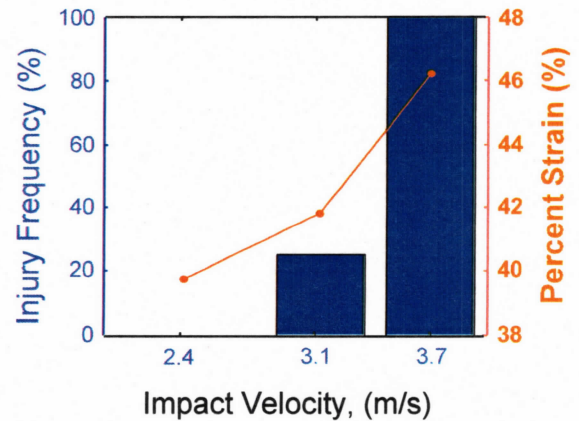
## Upper vessel strain, 3 drop heights



## Evidence of intima-intima contact



## Finite Element Model vs. Experiment



## Discussion: Model results vs. literature

- Finite element model strain approaches published values in the literature

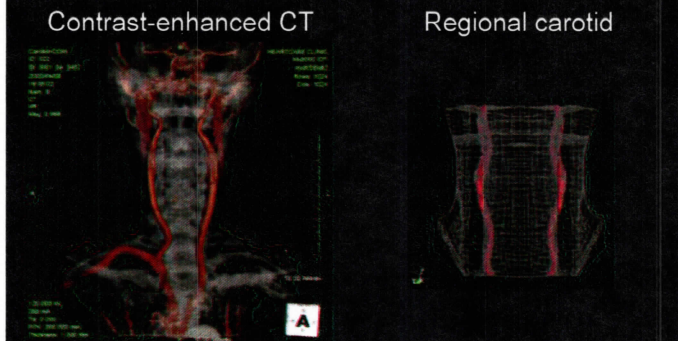
Loading Rate	Tissue	Diameter (mm)	Pre-conditioning	Strain to sub-failure (true, %)
Quasi-static	Porcine descending aorta	8.5±1.5	5 cycles @ 1 mm/sec	$\epsilon = 49$
Dynamic ~70 strain*sec <sup>-1</sup>	Porcine carotid artery	5.1±0.6	None	40 < $\epsilon$ < 46

## Study limitations

- Experimental design precludes direct validation of arterial strain
- Model should include strain rate dependency:
  - FE model strain rate of >70 strain•sec<sup>-1</sup>
  - Aorta test up to 80 strain•sec<sup>-1</sup>
    - (Mohan and Melvin, 1982, J. Biomech.)
  - Arterial sub-failure tested at 30 strain•sec<sup>-1</sup>
    - (Stemper et al., J Biomech., in press)

## Current and future research

Regional level model development and validation:



## Acknowledgments

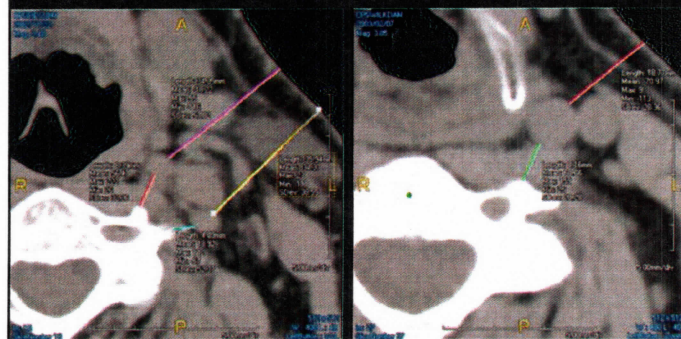
- Collaborators:
  - Dr. Brian Stemper and Dr. Frank Pintar, Medical College of Wisconsin
  - Josh Tan, Wake Forest University Baptist Medical Center
- Funding:
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  - Department of Veterans Affairs Medical Research

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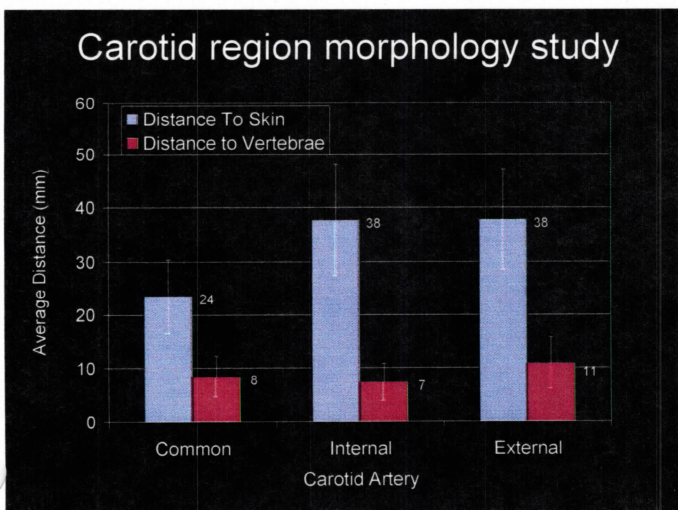
## Ongoing Research

## Current research

- Further organ level validation: Quantifying soft tissue thickness in cervical region

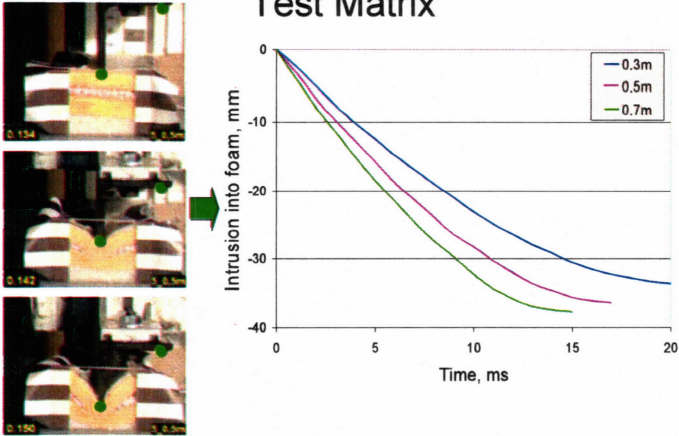


## Carotid region morphology study

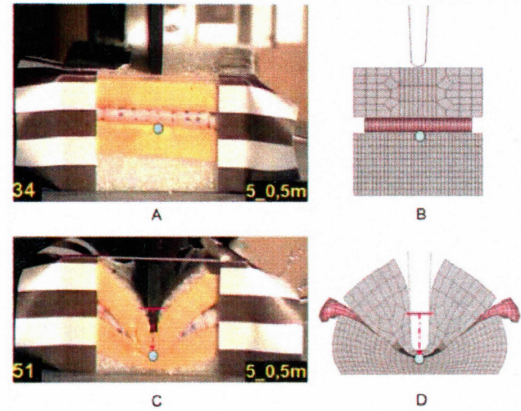


## Model validation slides

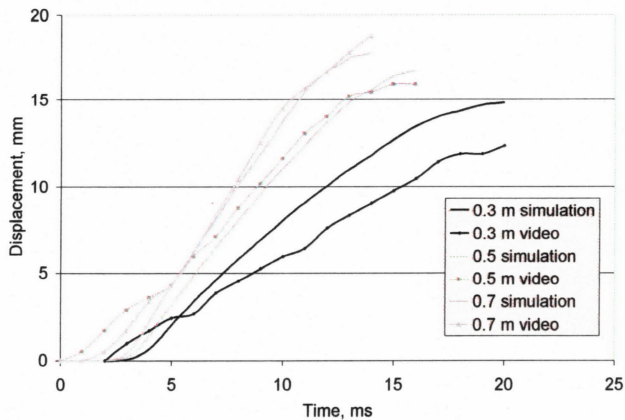
## Indenter Motion Profile Test Matrix



## Foam motion profile



## Foam motion profile

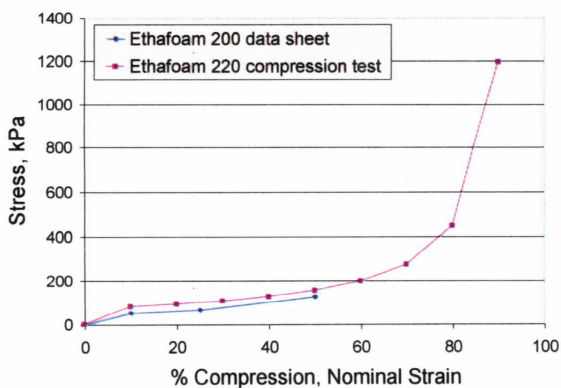


## Foam Material Model Summary

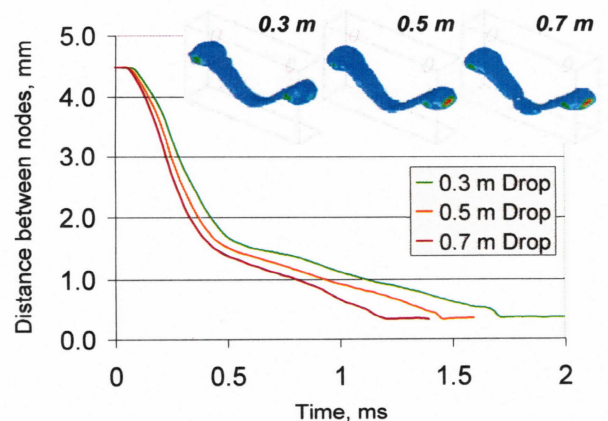
- \*MAT\_low\_density\_foam
  - Direct curve fit model
- Solid elements
- Use **load curve** to define nominal stress strain curve
- DAMP –Viscous coefficient to model damping

$\rho$	$36 \times 10^{-6}$	$\text{g/mm}^3$
E	0.236	MPa, [N/mm <sup>2</sup> ]
DAMP	0.5	

## Material Model - Foam



## Evidence of intima-intima contact

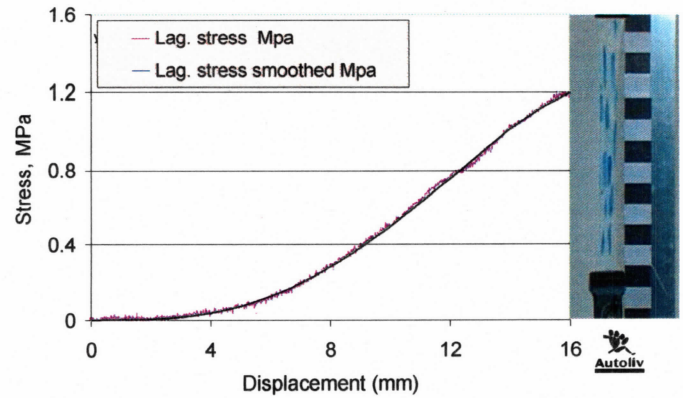


## Material model summary

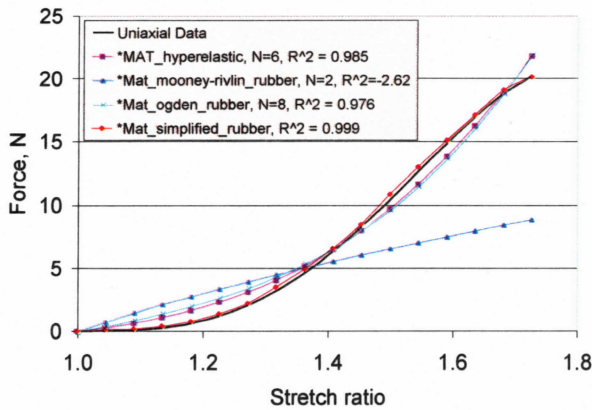
- \*MAT\_simplified\_rubber
  - Direct curve fit model
- Shell elements
- Model is robust
  - Parameter study
  - Mesh density study
- Strain rate effects and damage can be incorporated
  - Enter curves at discrete strain rates
  - Damage function can be implemented

$\rho$	0.001	g/mm <sup>3</sup>
K	2610	MPa, [N/mm <sup>2</sup> ]
G	5.2	MPa, [N/mm <sup>2</sup> ]
SIGF	5.2	kPa, [N/mm <sup>2</sup> ]
HG	Stiffness	

## Material Model - Artery



## Tissue level validation



# Material Model and Mathematics

## Finite element model of impact test

